



The Merits of the Integral Equation Methods in Computational Optoelectronics

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2. Fundamentals of Analytical Regularization

Reduction of EM BVP to a Fredholm's operator equation

Boundary-value problem

- Maxwell equations
- Boundary conditions
- Edge condition
- Radiation condition



- Integral equations
- Series equations

$$GX = Y$$



$$G = G_1 + G_2$$

Suppose that:

$$X + AX = B$$

$$A = G_1^{-1}G_2, \quad B = G_1^{-1}Y$$



G_1 is more singular than G_2

$$\|A\|_{L_2} < \infty, \quad B \in L_2$$

and G_1^{-1} is known



Fredholm 2-nd kind IE or infinite-matrix equation



3. Consequences of Regularization

Fredholm's theorems

$$X + A(k)X = B$$

Existence of exact solution:

If operator equation is equivalent to BVP, then its solution is unique for all real wavenumbers k



$$X = (I + A(k))^{-1} B$$

Point-wise convergence of discrete solutions:

$$e(N) = \|X - X^N\| (\|X\|)^{-1} \\ \leq \| (I + A)^{-1} \| \cdot \| A - A^N \| \xrightarrow{N \rightarrow \infty} 0$$

Condition number is stable:

$$\text{cond}(I + A) = \|I + A\| \cdot \| (I + A)^{-1} \| < \infty$$



4. Efficient Regularization Schemes

What is invertible?

$$G \xrightarrow{\text{Green arrow}} G = G_1 + G_2 \quad ?G_1$$

• Canonical-shape part (circular-cylinder & sphere)

well developed – trigonometric basis; used for multiple canonical scatterers & in a layered host medium

Small-contrast part

well developed – Muller equations, (loaded) volume IE

• Static part: PEC and imperfect zero-thickness screens

well developed – EFIE + Chebyshev basis in 2-D; variants – in FT domain, RHP (in periodic case)

• HF (halfplane) part: PEC and imperfect screens

scarcely developed – most promising for solving big problems of quasioptics with economic algorithms

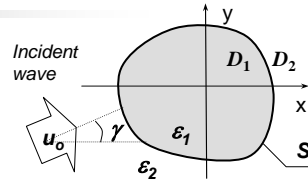




5. Dielectric Cylinder Scattering - Formulation

Boundary-value problem

Scattering by an arbitrary smooth dielectric cylinder. Incident field is a plane wave in the reception mode and a directive localized source field in the transmission mode



wavenumber $k_j = k\sqrt{\epsilon_j\mu_j}$ $\alpha_j = 1/\mu_j$ or $1/\epsilon_j$

2D BVP: Find $u_j(\vec{r})$, $r \in D_j$ $j=1,2$, **such that**

1. Helmholtz equation off S: $(\Delta + k_j^2)u_j^{sc}(\vec{r}) = 0$

2. Boundary conditions at S:

$$u_1(\vec{r})|_S = u_2(\vec{r})|_S \quad \text{and} \quad \alpha_1 \frac{\partial u_1(\vec{r})}{\partial n} \Big|_S = \alpha_2 \frac{\partial u_2(\vec{r})}{\partial n} \Big|_S$$

3. Sommerfeld radiation condition



6. Muller's Boundary Integral Equations

Small contrast inversion

Fields representation = combination of the single and double layer potentials

$$u_1(\vec{r}) = \int_S \left[p_1(\vec{r}_s) \frac{\partial G_1(\vec{r}, \vec{r}_s)}{\partial n_s} - q_1(\vec{r}_s) G_1(\vec{r}, \vec{r}_s) \right] dl_s \quad \vec{r} \in D_1$$

$j = 1, 2$

$$u_2(\vec{r}) = \int_S \left[q_2(\vec{r}_s) G_2(\vec{r}, \vec{r}_s) - u_2(\vec{r}_s) \frac{\partial G_2(\vec{r}, \vec{r}_s)}{\partial n_s} \right] dl_s + u_0(\vec{r}) \quad \vec{r} \in D_2$$

Parameterization + Boundary conditions =>

Uniquely solvable set of BIEs of the Fredholm 2nd kind :

$$\begin{cases} p_1(t) - \int_0^{2\pi} p_1(t_s) A(t, t_s) dt_s + \int_0^{2\pi} q_1(t_s) B(t, t_s) dt_s = L(t) u_0(t) \\ \left(1 + \frac{\alpha_1}{\alpha_2} \right) \frac{q_1(t)}{2} - \int_0^{2\pi} p_1(t_s) C(t, t_s) dt_s + \int_0^{2\pi} q_1(t_s) D(t, t_s) dt_s = L(t) \frac{\partial u_0(t)}{\partial n} \end{cases}$$

$$\alpha_j = \mu_j \quad \text{or} \quad \epsilon_j \quad \text{for E- or H-polarization}$$





7. Muller's Boundary Integral Equations

Kernel properties & discretization

In one of the kernels, a **log-type singularity is kept; others are regular**

$$A(t, t_s) = L(t) \left(\frac{\partial G_1}{\partial n_s} - \frac{\partial G_2}{\partial n_s} \right) \quad B(t, t_s) = L(t) \left(G_1 - \frac{\alpha_1}{\alpha_2} G_2 \right) \quad C(t, t_s) = L(t) \left(\frac{\partial^2 G_1}{\partial n_s \partial n} - \frac{\partial^2 G_2}{\partial n_s \partial n} \right)$$

$$\|A\|, \dots, \|D\| < (\varepsilon - 1) \text{Const} \quad D(t, t_s) = L(t) \left(\frac{\partial G_1}{\partial n} - \frac{\alpha_1}{\alpha_2} \frac{\partial G_2}{\partial n} \right)$$

Computing the singular integrals is improved by adding and subtracting the canonical-circle operators, e.g. G^0

$$G^0 = \frac{i}{4} H_0(2ka \text{Sin}[(t - t_s)/2])$$

MBIEs + trigonometric-Galerkin discretization
=> Fred.-2 Matrix Equation filled in with DDFT

$$p(t)L(t) = \frac{2}{i\pi} \sum_{m=-\infty}^{\infty} p_m e^{imt}$$



$$\begin{cases} \sum_{m=-\infty}^{\infty} p_m (\delta_{km} + A_{km}) + \sum_{m=-\infty}^{\infty} q_m B_{km} = u_k \\ \sum_{m=-\infty}^{\infty} p_m C_{km} + \sum_{m=-\infty}^{\infty} q_m (\delta_{km} + D_{km}) = \bar{u}_k \end{cases}$$

If the natural parameterization is used: $L(t)=1$



8. MBIE Algorithm Properties

Test example: super-ellipse

Homogeneous dielectric cylinder:

«super-ellipse» = rectangle with smoothed edges:

$$(x/la)^{2\nu} + (y/a)^{2\nu} = 1 \quad 0 < \nu < \infty$$

Relative computational error, determined by norm in l_2

$$e(N) = \frac{\|Z^N - Z^{N+1}\|}{\|Z^N\|}$$

where

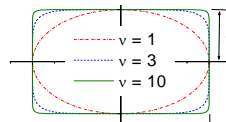
$$Z^N = \{z_n^{1N}, z_n^{2N}\}$$

3 digit accuracy is achieved if

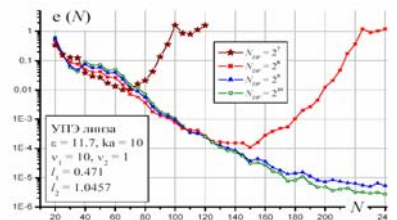
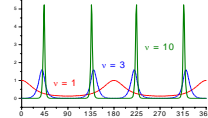
$$N \approx ka \sqrt{\varepsilon} + \nu + 10$$



"super-ellipse" cross-section



"super-ellipse" curvature



Computational error versus matrix block size N



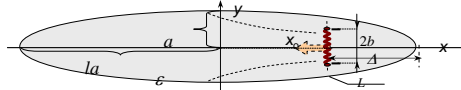
9. Radiation of a Dielectric Rod Antenna

Far-field characteristics: pattern, radiated power & directivity

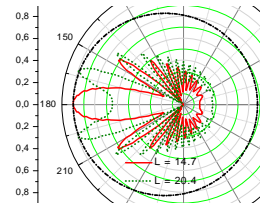
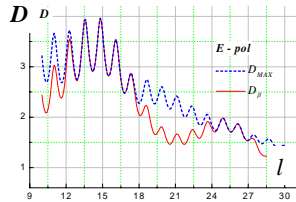
$$\Phi(\varphi) = \frac{1}{2\pi} \sum_{n=-\infty}^{\infty} p_n \int_0^{2\pi} e^{-ik(\cos(\varphi)x(t_s) + \sin(\varphi)y(t_s))} \cdot e^{int_s} dt_s$$

$$P^{rad} = \alpha_0 \frac{2}{\pi} \int_0^{2\pi} |\Phi(t)|^2 dt$$

$$D(\varphi) = 2\alpha_0 |\Phi(\varphi)|^2 \cdot (kP^{rad})^{-1}$$



Elliptic rod geometry and notations:
curvy line is the CSP feed aperture,
"l" is the elongation (axes ratio)



Directivity versus the rod elongation; dashed = in the main lobe, solid = along the axis ($\varphi = \beta$). $ka = 1$, $\epsilon = 2.5$, $\nu = 1$, $kb = 0.1$, $\beta = \pi$, $\Delta/a = 0.7$; $y_0/a = 0$.

Normalized Radiation Pattern



10. Wave Focusing by Elliptic-Front Lenses

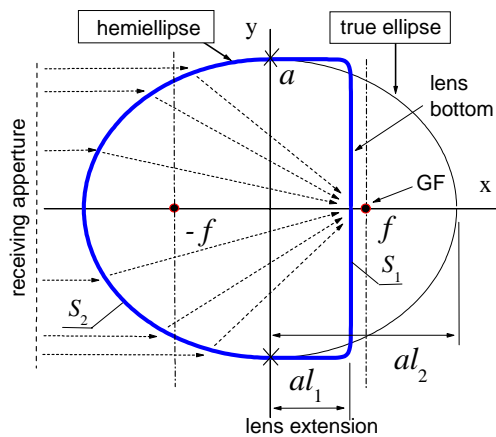
Geometry & Principle

Cross-sectional contour: $S = S_1 \cup S_2$

twice-continuous curve combined from smoothly joined halves of ellipse and super-ellipse

GO: Parallel rays come to the rear focus of the ellipse if the eccentricity is

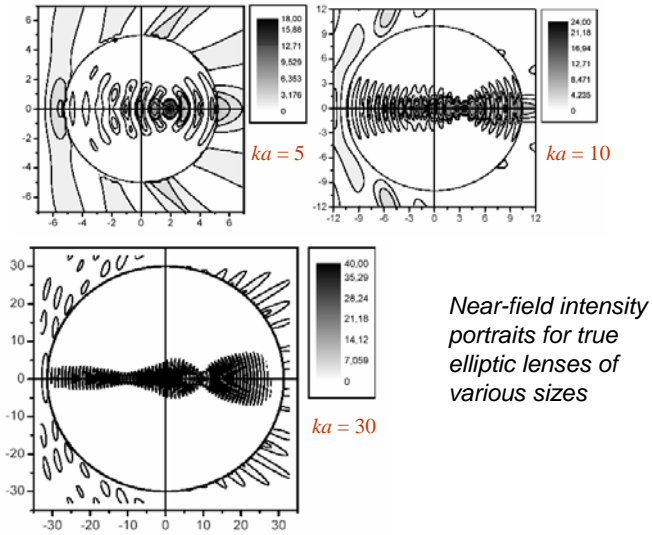
$$e = 1/\sqrt{\epsilon}$$





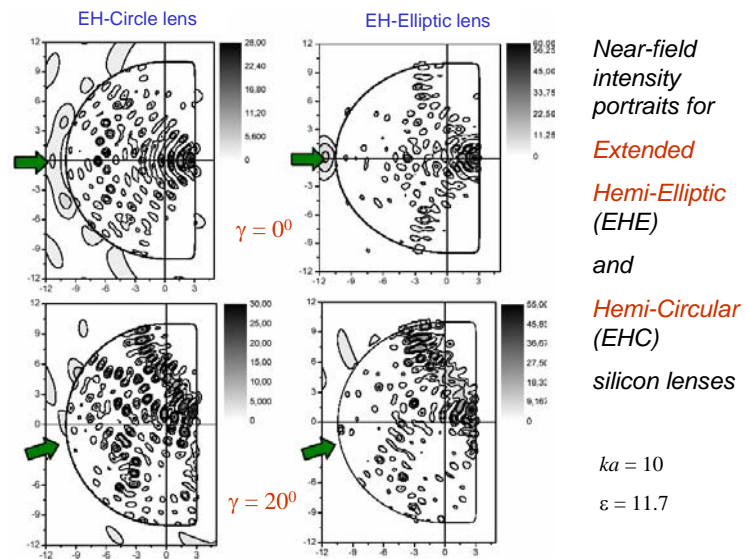
11. Wave Focusing by Elliptic Lenses

Near field characteristics



12. Wave Focusing by Elliptic-Front Lenses

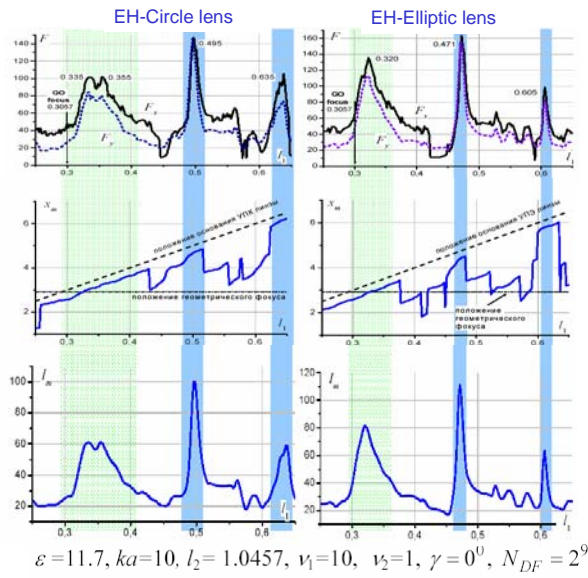
Near field characteristics





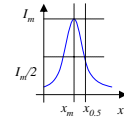
13. Wave Focusing by Elliptic-Front Lenses

Near field characteristics



Focusability vs l_1

$$F_{x,y} = \frac{al(x_n, y_m)}{|x, y_m - x, y_{0.5}|}$$



Main focus x-coordinate vs l_1

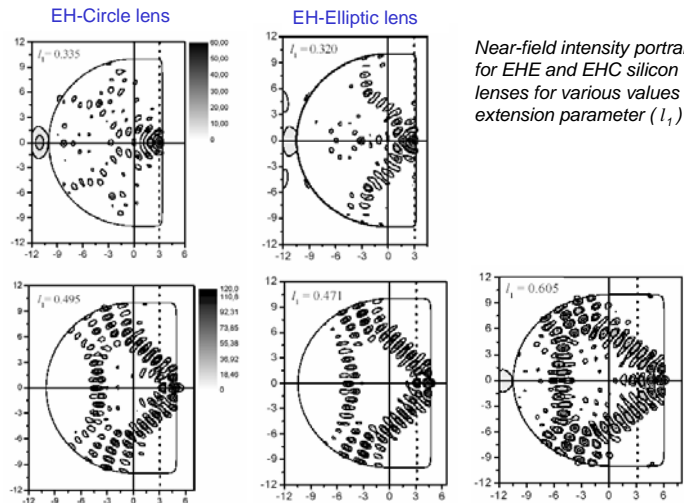


max intensity vs l_1



14. Wave Focusing by Elliptic-Front Lenses

Near field characteristics



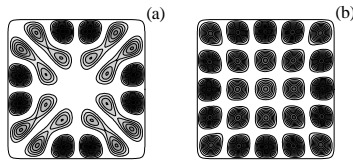
$$\varepsilon = 11.7, ka = 10, l_2 = 1.0457, \nu_1 = 10, \nu_2 = 1, \gamma = 0^0, N_{DF} = 2^{10}$$





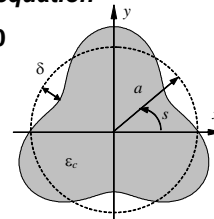
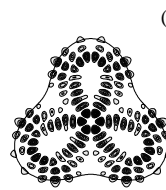
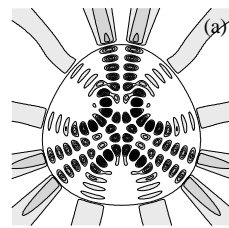
15. Natural Modes of Microcavities

Near fields of modes in open 2-D dielectric resonators



Eigenfrequency boundary-value problem => Muller's boundary integral equations => analytical extraction of circular-contour part => determinant equation

$$\text{Det} (I+A(k))=0$$



Modes in a square cavity with rounded edges (superellipse with $\nu=10$) and in a curved triangular cavity

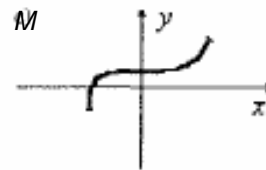
Refractive index is 2.63



16. PEC Strip Scattering - Formulation

Boundary-value problem

Scattering by an arbitrary smooth open cylindrical PEC strip. Incident field is a **plane wave in the RCS analysis** and a **directive localized feed field in the reflector antenna analysis**



2-D BVP: find such $u^{sc}(\vec{r})$, $u = u^{in} + u^{sc}$ **that**

1. Helmholtz equation off M : $(\Delta + k^2)u^{sc}(\vec{r}) = 0$

2. Boundary conditions at M :

$$u(\vec{r})|_M = 0, \quad E - \text{pol.} \quad \frac{\partial u(\vec{r})}{\partial n}|_M = 0, \quad H - \text{pol.}$$

3. Sommerfeld radiation condition

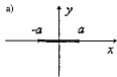




17. Electric-Field Integral Equations

Singular Integral Equations

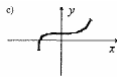
Fields representation – **single/double layer potential**:



E-pol.

H-pol.

$$u(\vec{r}) = \int_M p(\vec{r}_s) G_0(\vec{r}, \vec{r}_s) dl_s, \quad u(\vec{r}) = \int_M q(\vec{r}_s) \frac{\partial}{\partial n_s} G_0(\vec{r}, \vec{r}_s) dl_s$$



$$G_0(\vec{r}, \vec{r}_s) = \frac{i}{4} H_0^{(1)}(k |\vec{r} - \vec{r}_s|) \quad \text{Free space Green's function}$$

Parameterization of contour $M \Rightarrow$ Boundary conditions \Rightarrow **Singular IEs of the 1st kind**

E-polarization

H-polarization

$$\int_{-1}^1 p(t_s) G_0(t, t_s) L(t_s) dt_s = -u^{in}(t), \quad \frac{\partial}{\partial n} \int_{-1}^1 q(t_s) \frac{\partial}{\partial n_s} G_0(t, t_s) L(t_s) dt_s = -\frac{\partial u^{in}(t)}{\partial n}$$

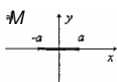


Direct discretization of SIE does not guarantee convergence, is inefficient and inaccurate



18. EFIE & Method of Analytical Preconditioning

Static-part inversion: diagonalization with eigenfunctions



Green's function decomposition = **static singular** part + regular part

$$G_0(\vec{r}, \vec{r}_s) = \frac{i}{4} \ln |\vec{r} - \vec{r}_s| + R(k |\vec{r} - \vec{r}_s|)$$

E-pol.

$$\int_{-1}^1 \frac{T_n(t_s)}{(1-t_s)^{1/2}} \ln(t-t_s) dt_s = \sigma_n T_n(t), \quad T_n(t) = \text{Chebyshev polynomials of the 1-st kind}$$

H-pol.

$$\int_{-1}^1 (1-t_s)^{1/2} U_n(t_s) \frac{\partial^2 \ln(\vec{r} - \vec{r}_s)}{\partial n^2} \Big|_M dt_s = \tau_n U_n(t), \quad U_n(t) = \text{Chebyshev polynomials of the 2-nd kind}$$



To transform SIE to the Fredholm 2nd kind matrix equation, take full set of the corresponding polynomials as a basis (i.e., make analytical preconditioning)

$$A X = B$$

\Downarrow

$$X + C X = D$$



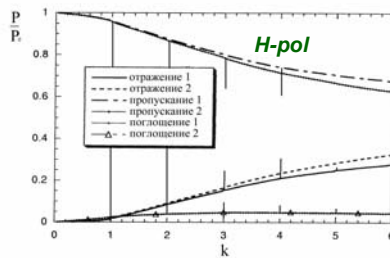
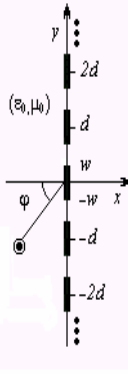
19. Scattering by a Dielectric Strip Grating

Static-part inversion: diagonalization with eigenfunctions

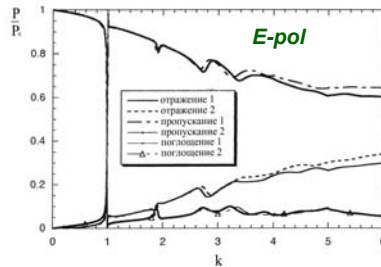
Generalized boundary conditions on *thin dielectric strips*:

$$(\vec{E}_T^+ + \vec{E}_T^-) = 2R(\vec{H}_T^+ - \vec{H}_T^-), \quad (\vec{H}_T^+ + \vec{H}_T^-) = 2Q(\vec{E}_T^+ - \vec{E}_T^-)$$

where $R = Q\zeta_r^2 = (i/2)\zeta_0\zeta_r \operatorname{ctg}(\sqrt{\epsilon_r\mu_r}k_0\tau/2)$



Fractions of transmitted, reflected and absorbed power versus normalized frequency, $\epsilon_r=10+i$, $\varphi=0^\circ$, $2w/d=0.5$, $\tau/d=0.01$.



Fractions of transmitted, reflected and absorbed power versus normalized frequency, $\epsilon_r=10+i$, $\varphi=0^\circ$, $2w/d=0.5$, $\tau/d=0.01$.

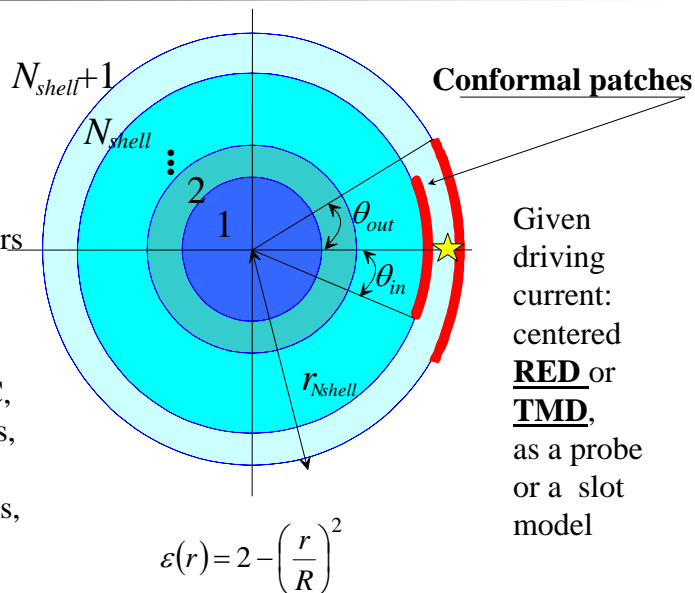


20. Radiation of Discrete Luneburg Lens Fed by Conformal Feed



Lens:
concentric
spherical layers
of uniform
dielectrics

Patches: PEC,
zero-thickness,
co-axial
spherical disks,
 $0 \leq \theta \leq \pi$



Given
driving
current:
centered
RED or
TMD,
as a probe
or a slot
model

21. Radiation of Discrete Luneburg Lens Fed by Conformal Feed

SCMA structure :

$$\theta_{in} = 0.02^\circ,$$

$$\theta_{out} = 0.04^\circ$$

$$r_{in}/r_{out} = 0.999$$

"large lens"

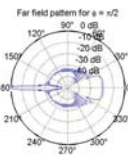
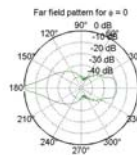
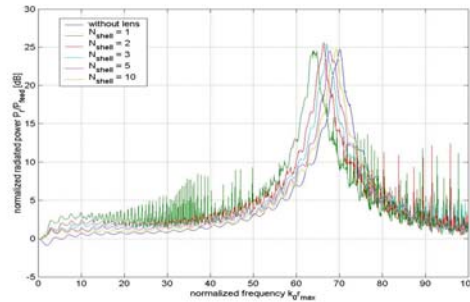
Lens structure :

N_{shell} : number of shells

$$\theta_i = 0, r_i = i/N_{shell}$$

$$\epsilon_{ri} = 2 - [(2i-1)/2N_{shell}]^2$$

$$\forall i, 1 \leq i \leq N_{shell}$$



Lens => small shift of SCMA resonance + whispering-gallery modes

22. Conclusions: Merits of Analytical Regularization of Integral Equations

1. Generates convergent and economic scattering algorithms with easily controlled accuracy
2. Leads to reliable simulations that predict even finest field features
3. Easily accesses quasioptical range
4. Is promising for CG iterative solvers
5. Can serve as a fast core for optimization
6. Enables explicit asymptotic solutions
7. Reduces eigenvalue problems to favorable determinant equations

